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Jameco Part Number 2056569

EVALUATION KIT AVAILABLE Adjustable-Output, Switch-Mode **Current Sources with Synchronous Rectifier**

General Description

The MAX1640/MAX1641 CMOS, adjustable-output. switch-mode current sources operate from a +5.5V to +26V input, and are ideal for microprocessor-controlled battery chargers. Charging current, maximum output voltage, and pulse-trickle charge are programmed with external resistors. Programming the off-time modifies the switching frequency, suppressing undesirable harmonics in noise-sensitive circuits. The MAX1640's highside current sensing allows the load to connect directly to ground, eliminating ground-potential errors. The MAX1641 incorporates a low-side current sense.

The MAX1640/MAX1641 step-down pulse-width-modulation (PWM) controllers use an external P-channel MOSFET switch and an optional, external N-channel MOSFET synchronous rectifier for increased efficiency. An internal low-dropout linear regulator provides power for the internal reference and circuitry as well as the gate drive for the N-channel synchronous rectifier.

The MAX1640/MAX1641 are available in space-saving. 16-pin narrow QSOP packages.

Applications

Battery-Powered Equipment

Laptop, Notebook, and Palmtop Computers

Handy Terminals

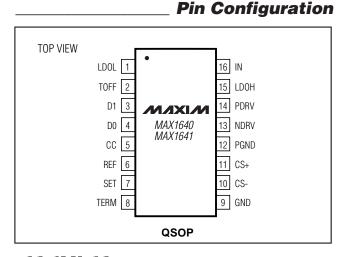
Portable Consumer Products

Cordless Phones

Cellular Phones

PCS Phones

Backup Battery Charger



Features

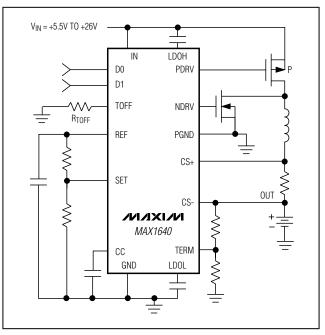
- ♦ 95% Efficiency
- ♦ +5.5V to +26V Input Supply Range
- ♦ 2V to 24V Adjustable-Output Voltage Range
- **♦ 100% Maximum Duty Cycle (Low Dropout)**
- ♦ Up to 500kHz PWM Operation
- **♦ Optional Synchronous Rectifier**
- ♦ 16-Pin QSOP Package
- ♦ Current-Sense Accuracy: 2% (MAX1641), 5.3% (MAX1640)

Ordering Information

PART	TEMP. RANGE	PIN-PACKAGE
MAX1640C/D	0°C to +70°C	Dice*
MAX1640EEE	-40°C to +85°C	16 QSOP
MAX1641C/D	0°C to +70°C	Dice*
MAX1641EEE	-40°C to +85°C	16 QSOP

^{*}Dice are specified at $T_A = +25$ °C, DC parameters only.

Typical Operating Circuit



MIXIM

Maxim Integrated Products 1

ABSOLUTE MAXIMUM RATINGS

V PGN	-0.3V to +28V PGND to GND	IN to GND
√ Con	+0.3V to -6V Continuous Po	LDOH to IN
V Q	0.3V to +6V QSOP (dera	LDOL to GND
) Ope	o (V _{IN} + 0.3V) Operating Tem	PDRV to GND
) M	$(LDOL + 0.3V)$ MAX164_EE	NDRV to GND
) Stor	(LDOL + 0.3V) Storage Temper	TOFF, REF, SET, TERM, C
√ Lead	0.3V to +6V Lead Tempera	D0, D1 to GND
/	0.3V to +28V	CS+, CS- to GND

PGND to GND	±0.3V
Continuous Power Dissipation (T _A = +70°C)	
QSOP (derate 8.30mW/°C above +70°C)	667mW
Operating Temperature Range	
MAX164_EEE	40°C to +85°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10sec)	+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

 $(V_{IN} = +12V, V_{OUT} = 6V, Circuit of Figure 2, T_A = 0^{\circ}C to +85^{\circ}C, unless otherwise noted. Typical values are at T_A = +25^{\circ}C.)$

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
Input Voltage Range	VIN			5.5		26	V
Linear-Regulator Output Voltage, V _{IN} Referenced	V _{LDOH}	V _{IN} = 5.5V to 26V, I _{LOAD} = 0 to 20mA		V _{IN} - 5.5	V _{IN} - 5.0	V _{IN} - 4.5	V
Linear-Regulator Output Voltage, Ground Referenced	V _{LDOL}	$V_{IN} = 5.5V \text{ to } 26V, I_L$	OAD = 0 to 20mA	4.5	5.0	5.5	V
Full-Scale Current-Sense		MAX1640		142	150	158	mV
Threshold		MAX1641		147	150	153	IIIV
Quarter-Scale Current-Sense		MAX1640		36	42	48	mV
Threshold		MAX1641		34	37.5	41	IIIV
Current-Sense Line Regulation		$V_{IN} = V_{OUT} + 0.5V to$	26V		0.03		%/V
Output Current Compliance		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	MAX1640		0.1	0.4	- %/V
Output Current Compliance		$V_{OUT} = 2V \text{ to } 24V$	MAX1641		0.1		
Oulogoopt V., Supply Current		D0 or D1 = high			2	4	mA
Quiescent V _{IN} Supply Current		D0 = D1 = low (off m	ode)		500		μΑ
Output Current in Off Mode		D0 = D1 = low				1	μΑ
V _{LDOL} Undervoltage Lockout				4.05	4.20	4.35	V
Reference Voltage	V _{REF}			1.96	2.00	2.04	V
Reference Load Regulation		$I_{REF} = 0$ to $50\mu A$			4	10	mV
V _{SET} Input Current						1	μΑ
FET Drive Output Resistance		PFET and NFET drive	9			12	Ω
Off-Time Range				1		10	μs
Off-Time Accuracy		$R_{TOFF} = 62k\Omega$		1.7	2.2	2.7	μs
Pulse-Trickle Mode Duty-Cycle Period		D0 = low, D1 = high, $R_{TOFF} = 100k\Omega$		27	33	40	ms
Pulse-Trickle Mode Duty Cycle (Note 1)		D0 = low, D1 = high,	$R_{TOFF} = 100k\Omega$		12.5		%

Note 1: This ratio is generated by a 1:8 clock divider and is not an error source for current calculations.

ELECTRICAL CHARACTERISTICS (continued)

 $(V_{IN} = +12V, V_{OUT} = 6V, Circuit of Figure 2, T_A = 0^{\circ}C to +85^{\circ}C, unless otherwise noted. Typical values are at T_A = +25^{\circ}C.)$

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
PWM Maximum Duty Cycle			100			%
Input Low Voltage	VIL	D0, D1			0.8	V
Input High Voltage	ViH	D0, D1	2.4			V
Input Leakage Current	I _{IN}	D0, D1			±1	μΑ

ELECTRICAL CHARACTERISTICS

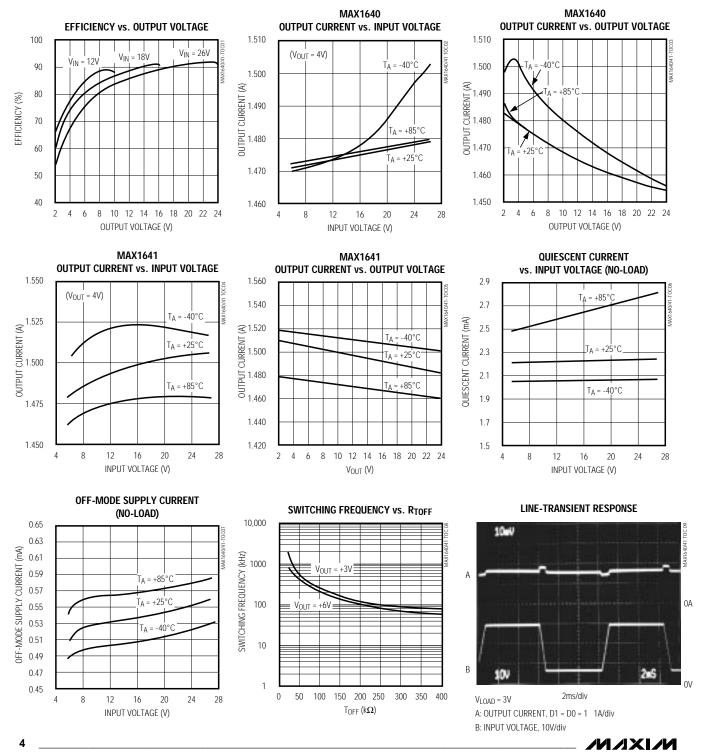
 $(V_{IN} = +12V, V_{OUT} = 6V, Circuit of Figure 2, T_A = -40^{\circ}C to +85^{\circ}C, unless otherwise noted.)$

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Input Voltage Range	VIN		5.5		26	V
Linear-Regulator Output Voltage, V _{IN} Referenced	V _{LDOH}	V _{IN} = 5.5V to 26V, I _{LOAD} = 0 to 20mA	V _{IN} - 5.5		V _{IN} - 4.5	V
Linear-Regulator Output Voltage, Ground Referenced	V _{LDOL}	V _{IN} = 5.5V to 26V, I _{LOAD} = 0 to 20mA	4.5		5.5	V
Full-Scale Current-Sense		MAX1640	141		159	mV
Threshold		MAX1641	146		154	IIIV
Quarter-Scale Current-Sense		MAX1640	34		48	mV
Threshold		MAX1641	33		42	IIIV
Output Current Compliance		V _{OUT} = 2V to 24V (MAX1640)			0.4	%/V
Quiescent V _{IN} Supply Current		D0 or D1 = high			4	mA
Output Current in Off Mode		D0 = D1 = low			1	μA
V _{LDOL} Undervoltage Lockout			4.0		4.4	V
Reference Voltage	V _{REF}		1.94		2.06	V
Reference Load Regulation		I _{REF} = 0 to 50µA			10	mV
V _{SET} Input Current					1	μΑ
FET Drive Output Resistance					12	Ω
Off-Time Range			1.5		8	μs
Off-Time Accuracy		$R_{TOFF} = 62k\Omega$	1.5		2.5	μs
Pulse-Trickle Mode Duty-Cycle Period		D0 = low, D1 = high, R _{TOFF} = $50k\Omega$	25		42	ms
PWM Maximum Duty Cycle			100			%
Input Low Voltage	VIL	D0, D1			0.8	V
Input High Voltage	V _{IH}	D0, D1	2.4			V
Input Leakage Current	I _{IN}	D0, D1			±1	μA



Typical Operating Characteristics

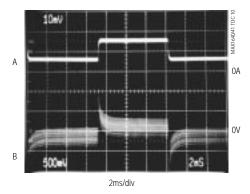
(Circuit of Figure 2, $T_A = +25$ °C, unless otherwise noted.)



Typical Operating Characteristics (continued)

(Circuit of Figure 2, $T_A = +25$ °C, unless otherwise noted.)

CURRENT-MODE CHANGE RESPONSE TIME



$$\begin{split} &V_{IN}=12V,\,V_{SET}=1V,\,R_{LOAD}=4\Omega,\,NO\ OUTPUT\ CAPACITOR\\ A:\ OUTPUT\ CURRENT,\,D0=D1=0\quad 1A/div\\ B:\ LOAD\ VOLTAGE,\,AC\ coupled,\,500mV/div \end{split}$$

A EXITING OFF MODE A 20µs/div

 V_{IN} = 12V, R_{LOAD} = 4 Ω A: D0 = D1 = 1 2V/div B: OUTPUT CURRENT, 0.5A/div

Pin Description

PIN	NAME	FUNCTION
1	LDOL	Internal, Ground-Referenced Low-Dropout Linear Regulator Output. Bypass with a 0.1µF capacitor in parallel with a 4.7µF capacitor to GND.
2	TOFF	Off-Time Select Input. A resistor (R _{TOFF}) connected from this pin to GND programs the off-time for the hysteretic PWM step-down converter. This resistor also sets the period in duty-cycle mode. See <i>Duty-Cycle Mode and Programming the Off-Time</i> .
3, 4	D1, D0	Digital Inputs. Select mode of operation (Table 1).
5	CC	Constant-Current Loop Compensation Input. Bypass with a 0.01µF capacitor to GND.
6	REF	Reference Voltage Output (V_{REF} = 2V). Bypass with a 0.1 μ F capacitor to GND.
7	SET	Current Select Input. Program the desired current level by applying a voltage at SET between 0V and V_{REF} , (I = V_{SET} / 13.3 R_{SENSE}). See Figure 3.
8	TERM	Maximum Output Voltage Termination Input. When V _{TERM} exceeds the reference voltage, the comparator resets the internal PWM latch, shutting off the external P-channel FET.
9	GND	Ground
10	CS-	Negative Current-Sense Comparator Input
11	CS+	Positive Current-Sense Comparator Input
12	PGND	High-Current Ground Return for the Output Drivers
13	NDRV	Gate Drive for an Optional N-Channel FET Synchronous Rectifier
14	PDRV	Gate Drive for the P-Channel FET
15	LDOH	Internal, Input-Referenced Low-Dropout Linear Regulator Output. Bypass with a 0.33µF capacitor to IN.
16	IN	Power-Supply Input. Input of the internal, low-dropout linear regulators.

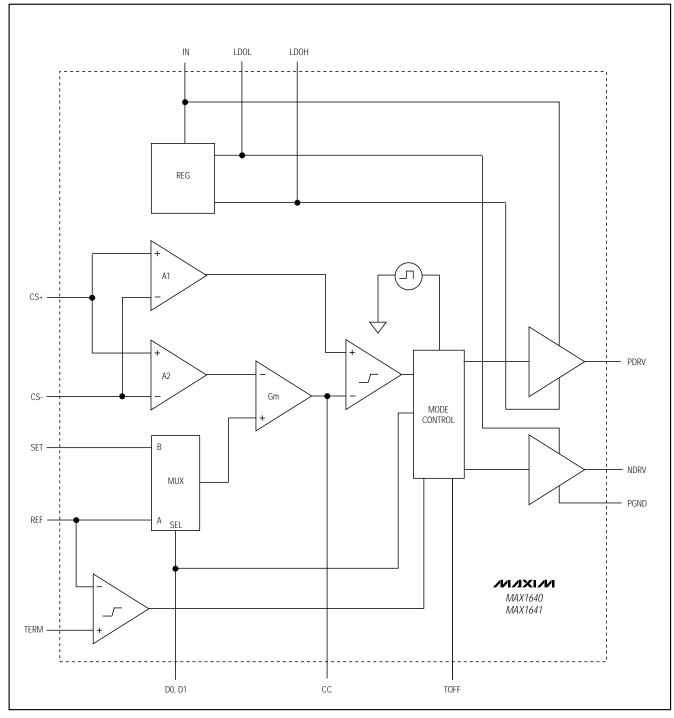


Figure 1. MAX1640/MAX1641 Functional Diagram

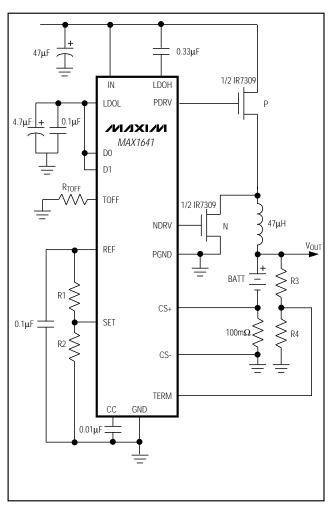


Figure 2a. Standard Application Circuit

Detailed Description

The MAX1640/MAX1641 switch-mode current sources utilize a hysteretic, current-mode, step-down pulse-width-modulation (PWM) topology with constant off-time. Internal comparators control the switching mechanism. These comparators monitor the current through a sense resistor (RSENSE) and the voltage at TERM. When inductor current reaches the current limit [(VCS+ - VCS-) / RSENSE], the P-channel FET turns off and the N-channel FET synchronous rectifier turns on. Inductor energy is delivered to the load as the current ramps down. This ramp rate depends on R_{TOFF} and inductor values. When off-time expires, the P-channel FET turns back on and the N-channel FET turns off.

Two digital inputs, D0 and D1, select between four possible current levels (Table 1). In pulse-trickle mode, the

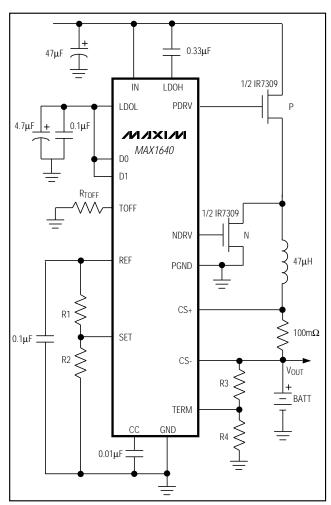


Figure 2b. Standard Application Circuit

part operates for 12.5% of the period set by R_{TOFF}, resulting in a lower current for pulse-trickle charging. Figure 1 is the MAX1640/MAX1641 functional diagram. Figure 2 shows the standard application circuits.

Charge Mode: Programming the Output Currents

The sense resistor, RSENSE, sets two charging current levels. Choose between these two levels by holding D0 high, and toggling D1 either high or low (Table 1). The fast-charge current level equals V_{CS} / RSENSE where V_{CS} is the full-scale current-sense voltage of 150mV. Alternatively, calculate this current by V_{REF} / (13.3RSENSE). The top-off current equals V_{SET} / (13.3RSENSE). A resistor-divider from REF to GND programs the voltage at SET (Figure 3).

The voltage at SET is given by:

R1 = R2 ($V_{REF} / V_{SET} - 1$); $10k\Omega < R2 < 300k\Omega$

where $V_{REF} = 2V$ and V_{SET} is proportional to the desired output current level.

Table 1. Selecting Output Current Levels

D1	DO	MODE	OUTPUT CURRENT (A)
0	0	OFF	0
0	1	Top-Off	V _{SET} / (13.3R _{SENSE})
1	0	Pulse-Trickle	V _{SET} / (13.3R _{SENSE}) 12.5% duty cycle
1	1	Fast Charge	V _{REF} / (13.3R _{SENSE})

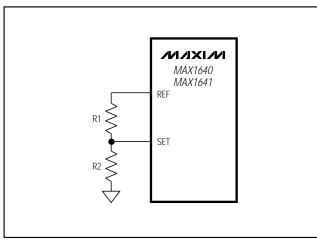


Figure 3. Adjusting the Output Current Level

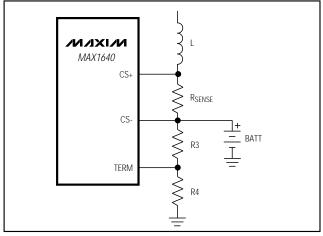


Figure 4a. Setting the Maximum Output Voltage Level

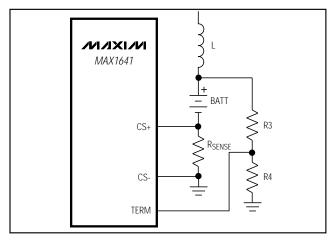


Figure 4b. Setting the Maximum Output Voltage Level

The MAX1640/MAX1641 are specified for VSET between 0V and VREF. For VSET > VREF, output current increases linearly (with reduced accuracy) until it clamps at VSET \approx 4V.

Pulse-Trickle Mode: Selecting the Pulse-Trickle Current

Pulling D0 low and D1 high selects pulse-trickle mode. This current equals V_{SET} / (13.3R_{SENSE}) and remains on for 12.5% of the period set by R_{TOFF}. Pulse-trickle current maintains full charge across the battery and can slowly charge a cold battery before fast charging commences.

PERIOD =
$$3.2 \times 10^{-7} \times R_{TOFF}(sec)$$

Off Mode: Turning Off the Output Current Pulling D0 and D1 low turns off the P-channel FET and hence the output current flow. This mode also controls end of charge and protects the battery against excessive temperatures.

Setting the Maximum Output Voltage Level

The maximum output voltage should be programmed to a level higher than the output/battery voltage (ILOAD x RLOAD). An external resistor-divider between the output and ground (Figure 4) sets the voltage at TERM. Once the voltage at TERM exceeds the reference, the internal comparator turns off the P-channel FET, terminating current flow. Select R4 in the $10k\Omega$ to $500k\Omega$ range. R3 is given by:

R3 = R4 (VOUT / VTFRM) -1

where $V_{TERM} = 2V$ and V_{OUT} is the desired output voltage.

Programming the Off-Time

When programming the off-time, consider such factors as maximum inductor current ripple, maximum output voltage, inductor value, and inductor current rating. The output current ripple is less than the inductor current ripple and depends heavily on the output capacitor's size.

Perform the following steps to program the off-time:

- 1) Select the maximum output current ripple. IR(A)
- 2) Select the maximum output voltage. VouT(MAX)(V)
- 3) Calculate the inductor value range as follows:

 $L_{MIN} = (V_{OUTMAX} \times 1\mu s) / I_{R}$

 $L_{MAX} = (V_{OUTMAX} \times 10 \mu s) / I_{R}$

- 4) Select an inductor value in this range.
- 5) Calculate toff as follows:

$$t_{OFF} = \frac{L \times I_R}{V_{OUTMAX}}$$

6) Program toff by selecting Rtoff from:

RTOFF =
$$(29.3 \times 10^9) \times toff$$

7) Calculate the switching frequency by:

$$fs = 1 / (t_{ON} + t_{OFF})$$

where $t_{ON} = (I_R \ x \ L) \ / \ (V_{IN} \ - \ V_{OUT})$ and $I_R = (V_{OUT} \ x \ t_{OFF}) \ / \ L$. L is the inductor value, V_{IN} is the input voltage, V_{OUT} is the output voltage, and I_R is the output peak-to-peak current ripple.

Note that R_{TOFF} sets both the off-time and the pulse-trickle charge period.

Reference

The on-chip reference is laser trimmed for a precise 2V at REF. REF can source no more than 50μ A. Bypass REF with a 0.1μ F capacitor to ground.

Constant-Current Loop: AC Loop Compensation

The constant-current loop's output is brought out at CC. To reduce noise due to variations in switching currents, bypass CC with a 1nF to 100nF capacitor to ground. A large capacitor value maintains a constant average output current but slows the loop response to changes in switching current. A small capacitor value speeds up the loop response to changes in switching current,

generating increased ripple at the output. Select C_{CC} to optimize the ripple vs. loop response.

Synchronous Rectification

Synchronous rectification reduces conduction losses in the rectifier by shunting the Schottky diode with a low-resistance MOSFET switch. In turn, efficiency increases by about 3% to 5% at heavy loads. To prevent cross-conduction or "shoot-through," the synchronous rectifier turns on shortly after the P-channel power MOSFET

Table 2. Component Manufacturers

COMPONENT	MANUFACTURER			
	Sumida	CDRH125 series		
Inductor	Coilcraft	D03316P series		
	Coiltronics	UP2 series		
MOSFETS	International Rectifier	IRF7309		
IVIOSI LTS	Siliconix	S14539DY		
Sense Resistor	Dale	WSL-2010 series		
Selise Resisiol	IRC	LR2010-01 series		
Capacitors	AVX	TPS series		
Capacitors	Sprague	595D series		
	Motorola	MBAR5340t3		
Rectifier	IVIOLOI OIA	IN5817-IN5822		
	Nihon	NSQ03A04		

turns off. The synchronous rectifier remains off for 90% of the off-time. In low-cost designs, the synchronous rectifier FET may be replaced by a Schottky diode.

Component Selection

External Switching Transistors

The MAX1640/MAX1641 drive an enhancement-mode P-channel MOSFET and a synchronous-rectifier N-channel MOSFET (Table 2).

When selecting a P-channel FET, some important parameters to consider are on-resistance ($r_{DS(ON)}$), maximum drain-to-source voltage (V_{DS} max), maximum gate-to-source voltage (V_{GS} max), and minimum threshold voltage (V_{TH} min).

In high-current applications, MOSFET package power dissipation often becomes a dominant design factor. I2R power losses are the greatest heat contributor for both high-side and low-side MOSFETs. Switching losses affect the upper MOSFET only (P-channel), since the Schottky rectifier or the N-FET body diode clamps the switching node before the synchronous rectifier turns on.

Rectifier Diode

If an N-channel MOSFET synchronous rectifier is not used, a Schottky rectifier is needed. The MAX1640/

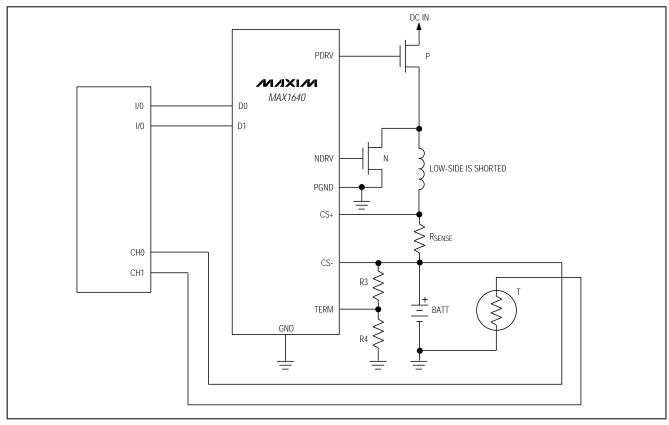


Figure 5. Microcontroller Battery Charger

MAX1641's high switching frequency demands a highspeed rectifier (Table 2). Schottky diodes such as the 1N5817-1N5822 are recommended. Make sure the Schottky diode's average current rating exceeds the peak current limit and that its breakdown voltage exceeds the output voltage (VOUT). For high-temperature applications, Schottky diodes may be inadequate due to their high leakage current; high-speed silicon diodes such as the MUR105 or EC11FS1 can be used instead. At heavy loads and high temperatures, the benefits of a Schottky diode's low forward voltage may outweigh the disadvantage of high leakage current. If the application uses an N-channel MOSFET synchronous rectifier, a parallel Schottky diode is usually unnecessary except with very high charge current (> 3 amps). Best efficiency is achieved with both an N-channel MOSFET and a Schottky diode.

Inductor Value

Refer to the section *Programming the Off-Time* to select the proper inductor value. There is a trade-off between inductor value, off-time, output current ripple, and switching frequency.

____Applications Information

All-Purpose Microcontroller Battery Charger: NiCd, NiMH

In applications where a microcontroller is available, the MAX1640/MAX1641 can be used as a low-cost battery charger (Figure 5). The controller takes over fast charge, pulse-trickle charge, charge termination, and other smart functions. By monitoring the output voltage at Vout, the controller initiates fast charge (set D0 and D1 high), terminates fast charge and initiates top-off (set D0 high and D1 low), enters trickle charge (set D0 low and D1 high), or shuts off and terminates current flow (set D0 and D1 low).

Layout and Grounding

Due to high current levels and fast switching waveforms, proper PC board layout is essential. High-current ground paths should be connected in a star

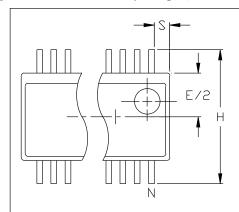
configuration to PGND. These traces should be wide to reduce resistance and as short as possible to reduce stray inductance. All low-current ground paths should be connected to GND. Place the input bypass capacitor as close as possible to the IN pin. See MAX1640 EV kit for layout example.

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TRANSISTOR COUNT: 1233

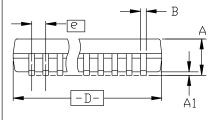
Package Information

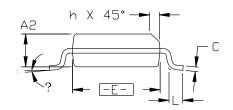
(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to www.maxim-ic.com/packages.)



	INCH	INCHES		IETERS	
DIM	MIN	MAX	MIN	MAX	
Α	.061	.068	1.55	1.73	
A1	.004	.0098	0.127	0.25	
Δ2	.055	.061	1.40	1.55	
В	.008	.012	0.20	0.31	
О	.0075	.0098	0.19	0.25	
D		SEE VA	RIATION:	S	
Ε	.150	.157	3.81	3.99	
е	.025	BSC	0.635 BSC		
I	.230	.244	5.84	6.20	
h	.010	.016	0.25	0.41	
L	.016	.035	0.41	0.89	
Ν	SEE VARIATIONS				
S	SEE VARIATIONS			2	
?:	0°	8*	0*	8*	

VΑ	RIATI	:2NC			
	INCHE	2	MILLIM	ETERS	
	MIN.	MAX.	MIN.	MAX.	N
D	.189	.196	4.80	4.98	16 AA
S	.0020	.0070	0.05	0.18	
D	.337	.344	8.56	8.74	20 AB
S	.0500	.0550	1.27	1.40	
D	.337	.344	8.56	8.74	24 AC
S	.0250	.0300	0.64	0.76	
_					
D	.386	.393	9.80	9.98	28 AD
S	.0250	.0300	0.64	0.76]





NOTES:

- 1. D & E DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS
- 2. MOLD FLASH OR PROTRUSIONS NOT TO EXCEED .006"
- 3. CONTROLLING DIMENSIONS: INCHES

PACKAGE DUTLINE, QSDP, .150 INCH, .025"

21-0055

Maxim cannot assume responsibility for use of any circuitry other than circuitry entirely embodied in a Maxim product. No circuit patent licenses are implied. Maxim reserves the right to change the circuitry and specifications without notice at any time.