

## MicroNote 010

---

### How to Quickly Obtain Spice Parameters for Diodes

---

By Kent Walters

Component SPICE modeling has become a frequently used analysis tool by design engineers to evaluate circuit performance. This MicroNote provides background information and methods useful for quickly obtaining many of the discrete diode SPICE parameters (such as  $BV$ ,  $IBV$ ,  $IS$ ,  $EG$ ,  $TBV1$ , etc.) from either specified datasheet parameters or other known information. Others may be approximated as described herein or obtained from the manufacturing source with other related physical design or characteristic background information. The SPICE parameters for diodes described in this MicroNote begin with the reverse diode characteristics and conclude with the forward parameter features. For quick reference, each of the SPICE parameter acronyms are underlined and are then described in further detail.

The first example of  $BV$  for reverse breakdown knee voltage simply approximates the avalanche breakdown voltage, or what has been identified in datasheets as  $V_{BR}$  for rectifiers and transient voltage suppressors (TVSs), or  $V_Z$  for zener diodes. If the  $V_{BR}$  parameter is not specified for rectifiers, it may be approximated as somewhat higher than the commonly rated reverse voltage ( $V_{RWM}$ ) of a rectifier. A 10% to 20% higher value is typical for fast and ultrafast rectifiers, or Schottkys. For lower voltage standard rectifiers in a JEDEC registered series where reverse recovery time is not critical (e.g., 1N4000 series), the actual  $V_{BR}$  can be many times higher than rated  $V_{RWM}$ . This occurs when rectifiers are downgraded from higher voltages in a series by a manufacturer where all other parameters (such as forward voltage) are identical in ratings.

The  $IBV$  that represents reverse breakdown knee current for onset of breakdown voltage can be approximated as ten times greater than the maximum specified leakage current ( $I_R$ ). In other examples for a conservative or worst-case (highest) value, this may instead be specified as  $I_{ZK}$  for knee current on zeners or  $I_{BR}$  (sometimes listed as  $I_T$ ) for TVS. It may also simply be those values shown separately for the  $V_{BR}$  current on some signal/switching diode datasheets. Many of these latter examples often specify the  $V_{BR}$  at 100  $\mu A$  that is applicable for  $IBV$ .

The saturation current  $IS$  may be approximated as the process norm of the leakage current in large-scale signal dc modeling with SPICE. This may be further represented in datasheets as  $I_R$  for rectifiers or zeners, and  $I_D$  for TVSs. For glass passivated pn junction designs (as primarily offered by Microsemi), this may typically be 10% to 20% of maximum leakage current specified for diodes in many of the 1Nxxxx JEDEC registrations. For a worst-case (highest value) scenario, it can also be simply modeled as the maximum leakage current  $I_R$  (or  $I_D$ ) value specified. This may be in the range of  $10^{-8}$  A to  $10^{-5}$  A depending on size of the diode. For low voltage zeners or TVSs that do not avalanche with a sharp knee region, the leakage current or saturation current approaches that of the rated maximum  $I_R$  of zeners or  $I_D$  of a TVS. This can sometimes approach 100  $\mu A$  to 5000  $\mu A$  ( $10^{-4}$  A to  $5 \times 10^{-3}$  A), again depending on size of the device.

If the  $IS$  value is needed for a linearized small-signal AC SPICE model, this would equate to smaller saturation current values when measured at 0.026 V ( $kT/q$ ). This results in very low  $IS$  values in the  $10^{-9}$  A to  $10^{-15}$  A range (or nA to fA), depending on size of the diode.

The zero bias pn junction capacitance  $CJO$  is also often specified in various diode datasheets. This may simply be shown as  $C$  if also stated at 0 V. If not, it will require direct measurement or further information from the manufacturing source. Much like a parallel plate capacitor, the diode capacitance will be dictated by its pn junction area size and depletion layer spread (or plate separation). This results in higher capacitance for larger size rectifiers (or Schottkys) as well as zeners and TVSs. It is similarly dependent on the actual voltage  $V_Z$  or  $V_{BR}$  (or effective plate separation). The higher the actual voltage, the lower the capacitance. This is particularly evident when comparing the capacitance for an overall family series listing of zeners or TVSs where low-voltage devices are depicted with much higher capacitance than high-voltage types.

The pn grading coefficient  $M$  further characterizes sensitivity of capacitance and its decline with applied reverse voltage on a logarithmic scale. It is not directly shown on datasheets, but the effective  $M$  values generally lie between the value of 0.25 to 0.45 for most conventional pn junction diodes. Low-voltage zeners below 5 V using alloy-diffused pn junction technology may only have an  $M$  value of 0.25, whereas higher voltage zeners (50 V to 100 V) may be 0.35. Higher voltage rectifiers of many hundreds of volts may approach 0.45. An abrupt junction or Schottky diode has an  $M$  value of 0.5 if there is no graded pn junction guard ring present. Modern Schottky rectifiers have pn guard rings typically resulting in  $M$  values of approximately 0.4.

The BV temperature coefficient (linear) of TBV1 is equivalent to the specified zener voltage temperature coefficient  $\alpha_{VZ}$  parameter, specified for most zeners as well as the breakdown voltage temperature coefficient  $\alpha_{V(BR)}$  for TVSs on numerous datasheets. For rectifiers, it approximates the same value as high-voltage zeners or TVSs, or approximately 0.11%/°C. This positive temperature coefficient (where  $V_{BR}$  increases with temperature) is also the reason that  $V_{BR}$  for rectifiers must be at least 10% or higher than rated voltage  $V_{RWM}$  at 25 °C when operating temperatures are reduced. This will ensure an operating temperature range down to -55 °C where  $V_{BR}$  also declines but still remains above  $V_{RWM}$  with this initial 10% design margin at 25 °C.

The parasitic resistance  $R_S$  is not a value directly given on datasheets. It is determined by the diode element contact resistance and bulk resistance  $R$  through the material of resistivity ( $\rho$ ), of area ( $A$ ), and length in current flow ( $L$ ) on either side of the pn junction. The length of this current flow is primarily related to semiconductor element thickness. The resistivity  $\rho$  also varies over this thickness as dictated by device geometry and diffusion profile. The effective resistance  $R$  is then primarily determined by the classic relation of  $R = \rho \times L / A$  that may be integrated over this thickness. It can also be measured with special test methods or acquired from the manufacturer.

One example of parasitic resistance effects on zeners or TVSs is described in [MicroNote 202](#). Small configured devices have higher  $R_S$  compared to large devices of the same voltage rating. Also, higher voltage devices will have higher  $R_S$  than low voltage due to higher resistivity material or thickness required for generating higher voltage  $V_Z$  or  $V_{BR}$  characteristics. These overall effects can result in large low-voltage zeners running as low as 0.001  $\Omega$ , whereas small geometry high-voltage rectifiers may run many  $\Omega$  in  $R_S$  value. Many diode types are typically in the range of 0.01  $\Omega$  to 0.1  $\Omega$ .

The  $R_S$  temperature coefficient TRS1 is often given a default value of zero; however, it is better approximated as 0.76%/°C for silicon if needed for critical circuit analysis in PSPICE regarding slight variations of  $R_S$  over a broad operating temperature range.

The transit time  $TT$  is often given a default value of zero when it is not considered a critical feature in circuit design. When needed, the  $TT$  value is a complex parameter to quantify for pn diodes since it is also dependent on the operating current and slew rate ( $di/dt$ ) similar to that observed for reverse recovery time ( $trr$ ). This may be further reviewed in [MicroNote 302](#) describing  $trr$ . The  $TT$  value may be approximated by a value somewhat greater than specified for  $trr$  in fast or ultrafast rectifier datasheets. It can be somewhat less than 10 ns for small signal or switching diodes, or in the range of approximately 50 ns for ultrafast rectifiers, or 250 ns in fast rectifiers. For zeners or TVSs where  $trr$  is not specified or controlled, this value typically varies from 200 ns for low-voltage types less than 10 V to as much as 3 ms for high-voltage devices exceeding 100 V, including standard rectifiers. For Schottky rectifiers, the  $TT$  value is zero.

The bandgap voltage (barrier height)  $EG$  is 1.11 eV for silicon pn diodes and typically 0.7 eV for Schottky diodes. Germanium diodes have an  $EG$  of 0.67 eV. Most diode types are silicon.

In rectifiers where forward voltage characteristics can also be important in SPICE modeling for circuit designs, the pn potential VJ for most diodes is considered 0.8 V in default value and the forward bias depletion capacitance coefficient FC is 0.5. The emission coefficient N can be used to modify the slope of the low-level forward current versus voltage I-V characteristics curve. Its default value is 1.0 and typical value is 1.1. In the high-level injection forward current region the slope is primarily determined by the resistive effects of the diode as influenced by the previously described RS parasitic resistance. To help identify these two regions, the forward knee current I<sub>kf</sub> models the intersecting asymptotes of low-to-high forward current injection versus forward voltage. When viewing typical forward current characteristics on a log scale versus linear forward voltage scale, this intersection or subtle inflection point for determining the value of I<sub>kf</sub> is often in the same vicinity as the average forward current rating I<sub>o</sub> for rectifiers.

Other SPICE parameters exist but these are the primary examples of interest for most applications. In summary, the descriptions provided herein may serve as a quick approximation method for many diode SPICE parameters and how they may vary based on specified parameters found in datasheets or as additionally provided by the manufacturing source.

## Support

For additional technical information, please contact Design Support at:

<http://www.microsemi.com/designsupport>

or

Kent Walters (kwalters@microsemi.com) at 480-302-1144

**Microsemi Corporate Headquarters**

One Enterprise, Aliso Viejo,  
CA 92656 USA  
Within the USA: +1 (800) 713-4113  
Outside the USA: +1 (949) 380-6100  
Fax: +1 (949) 215-4996  
Email: [sales.support@microsemi.com](mailto:sales.support@microsemi.com)  
[www.microsemi.com](http://www.microsemi.com)

© 2018 Microsemi Corporation. All rights reserved. Microsemi and the Microsemi logo are trademarks of Microsemi Corporation. All other trademarks and service marks are the property of their respective owners.

Microsemi makes no warranty, representation, or guarantee regarding the information contained herein or the suitability of its products and service for any particular purpose, nor does Microsemi assume any liability whatsoever arising out of the application or use of any product or circuit. The products sold hereunder and any other products sold by Microsemi have been subject to limited testing and should not be used in conjunction with mission-critical equipment or applications. Any performance specifications are believed to be reliable but are not verified, and Buyer must conduct any complete all performance and other testing of the products, alone and together with, or installed in, any end-products. Buyer shall not rely on any data and performance specifications or parameters provided by Microsemi. It is the Buyer's responsibility to independently determine suitability of any products and to test and verify the same. The information provided by Microsemi hereunder is provided "as is, where is" and with all faults, and the entire risk associated with such information is entirely with the Buyer. Microsemi does not grant, explicitly or implicitly, to any party any patent rights licenses, or any other IP rights, whether with regard to such information itself or anything described by such information. Information provided in this document is proprietary to Microsemi, and Microsemi reserves the right to make any changes to the information in this document or to any product and services at any time without notice.

Microsemi Corporation (Nasdaq: MSCC) offers a comprehensive portfolio of semiconductor and system solutions for aerospace & defense, communications, data center and industrial markets. Products include high-performance and radiation-hardened analog mixed-signal integrated circuits, FPGAs, SoCs and ASICs; power management products; timing and synchronization devices and precise time solutions, setting the world standard for time; voice processing devices; RF solutions; discrete components; enterprise storage and communication solutions; security technologies and scalable anti-tamper products; Ethernet solutions; Power-over-Ethernet ICs and midspans; as well as custom design capabilities and services. Microsemi is headquartered in Aliso Viejo, California, and has approximately 4,800 employees globally. Learn more at [www.microsemi.com](http://www.microsemi.com).